

On the numerical solution of a micropolar continuum model

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NSCM-26 Oslo, 23-25 October 2013



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Equilibrium equations

Force balance

$$\frac{\partial \sigma_{ji}}{\partial x_j} + \rho b_i = 0,$$

Moment balance

$$\frac{\partial \mu_{ji}}{\partial x_j} + \rho c_i + \epsilon_{ijk} \sigma_{jk} = 0,$$

σ force stress tensor

μ moment stress tensor

b body force per unit mass

c body moment per unit mass

ϵ_{ijk} alternating tensor

ρ the mass density

Constitutive equations

Linear material model

$$\sigma_{ij} = C_{ijkl}^{(\gamma)} \gamma_{kl}, \quad \mu_{ij} = C_{ijkl}^{(\kappa)} \kappa_{kl},$$

the Cosserat's first strain tensor γ_{ij} and microcurvature tensor κ_{ij} are

$$\gamma_{ij} = u_{j,i} - \epsilon_{kij} \varphi_k, \quad \text{and} \quad \kappa_{ij} = \varphi_{j,i},$$

φ is the microrotation field

The material stiffness tensors for an isotropic solid can be expressed as

$$C_{ijkl}^{(\gamma)} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) + \mu_c (\delta_{ik} \delta_{jl} - \delta_{il} \delta_{jk}),$$

$$C_{ijkl}^{(\kappa)} = \alpha \delta_{ij} \delta_{kl} + \beta (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) + \gamma (\delta_{ik} \delta_{jl} - \delta_{il} \delta_{jk}).$$

Comprehensible set of material parameters

the characteristic length in torsion

$$\ell_t = \sqrt{\frac{\beta}{\mu}},$$

the characteristic length in bending

$$\ell_b = \sqrt{\frac{\beta + \gamma}{4\mu}},$$

the coupling number

$$N = \sqrt{\frac{\mu_c}{\mu + \mu_c}},$$

and the polar ratio

$$\psi = \frac{\beta}{\beta + \frac{1}{2}\alpha}.$$

$$0 \leq N \leq 1, \quad \text{and} \quad 0 \leq \psi \leq \frac{3}{2},$$



Conformally invariant curvature state

Neff et al. 2009, 2010

$$\mu_{ij} = (\alpha + \frac{2}{3}\beta)\kappa_{kk}\delta_{ij} + 2\beta\kappa'_{(ij)} + 2\gamma\kappa_{[ij]}$$

$$\gamma_{(ij)} = \frac{1}{2}(\gamma_{ij} + \gamma_{ji}), \quad \gamma_{[ij]} = \frac{1}{2}(\gamma_{ij} - \gamma_{ji}).$$

The curvature tensor is symmetric and deviatoric

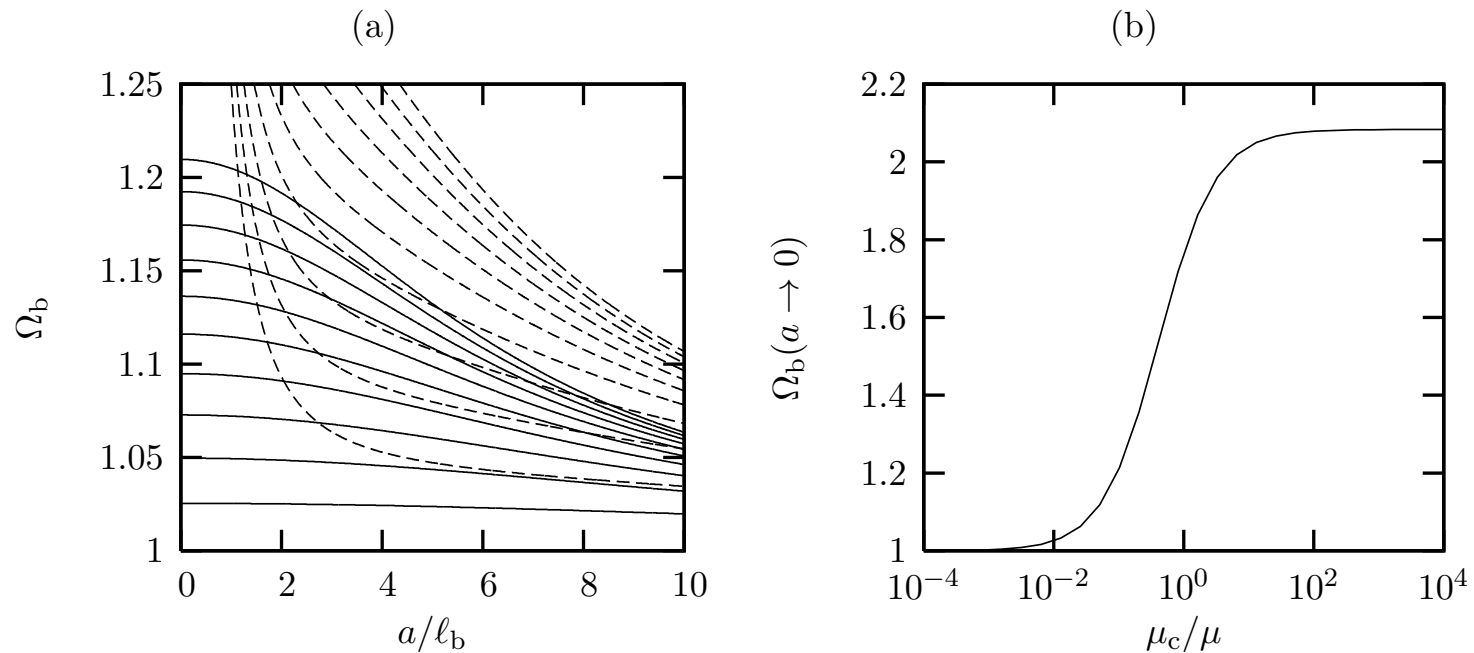
$$\gamma = 0, \quad \beta = \mu\ell_t^2, \quad \alpha = -\frac{2}{3}\mu\ell_t^2.$$

Four material parameters $\lambda, \mu, \mu_c, \ell_t$.



Size effect - pure bending of a beam

Circular cross-section with radius a



- (a) From bottom to top $\mu_c/\mu = 0.01, 0.02, 0.03, \dots, 0.09, 0.1$. Solid lines: conformally invariant curvature case ($\beta = 4\mu\ell_b^2, \gamma = 0$); dashed lines $\gamma = 0.01\beta$.
- (b) $\Omega_b(a \rightarrow 0)$ for the conformally invariant curvature state.

Numerical solution

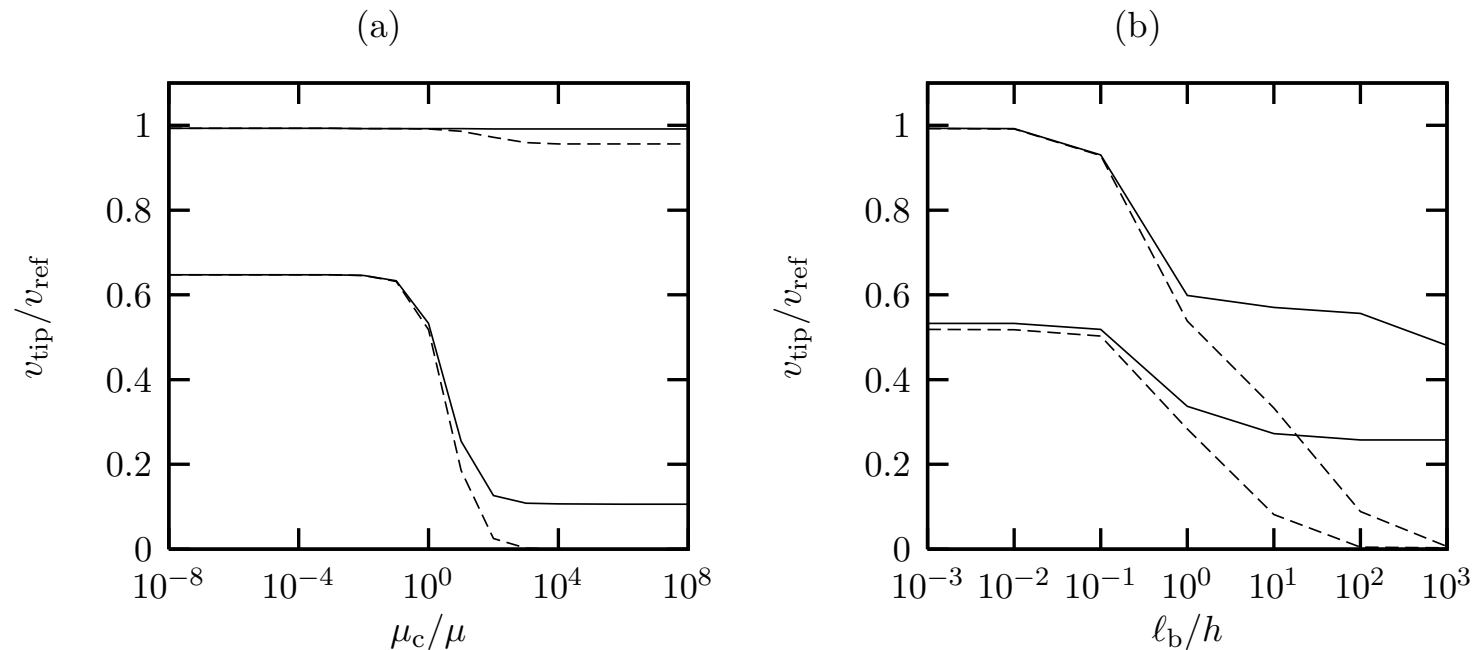
The virtual work expression

$$\int_V [(-\nabla \cdot \boldsymbol{\sigma}^T - \rho \mathbf{b}) \cdot \delta \mathbf{u} + (-\nabla \cdot \boldsymbol{\mu}^T - \boldsymbol{\epsilon} : \boldsymbol{\sigma} - \rho \mathbf{c}) \cdot \delta \boldsymbol{\phi}] \, dV = 0$$

$$\begin{aligned} \int_V [\boldsymbol{\sigma} : ((\nabla \delta \mathbf{u})^T - \text{skew}(\delta \boldsymbol{\varphi})) + \boldsymbol{\mu} : (\nabla \delta \boldsymbol{\varphi})^T] \, dV \\ - \int_V (\rho \mathbf{b} \cdot \delta \mathbf{u} + \rho \mathbf{c} \cdot \delta \boldsymbol{\varphi}) \, dV - \int_S (\mathbf{t} \cdot \delta \mathbf{u} + \mathbf{m} \cdot \delta \boldsymbol{\varphi}) \, dS = 0 \end{aligned}$$

Standard C_0 -interpolation for both u and φ .

Example - cantilever beam



(a) $\ell_b = h/200$. The upper two curves triquadratic elements and the lower ones with trilinear elements. Solid lines: rotations are free at the clamped edge, dashed lines: rotations are suppressed.

(b) The effect of internal length scale ℓ_b on the FE solution: $\mu_c = \mu$.

Concluding remarks

- Stable and locking free FE-formulation needed for the micropolar model.

Thanks!



Edvard Munch, Anxiety, 1894

Equilibrium equations in terms of displacements and rotations

$$\begin{aligned}(\lambda + \mu - \mu_c) \operatorname{grad} \operatorname{div} \mathbf{u} + (\mu + \mu_c) \Delta \mathbf{u} + 2\mu_c \operatorname{curl} \boldsymbol{\varphi} + \rho \mathbf{b} &= \mathbf{0} \\(\alpha + \beta - \gamma) \operatorname{grad} \operatorname{div} \boldsymbol{\varphi} + (\beta + \gamma) \Delta \boldsymbol{\varphi} - 4\mu_c \boldsymbol{\varphi} + 2\mu_c \operatorname{curl} \mathbf{u} + \rho \mathbf{c} &= \mathbf{0}\end{aligned}$$

$$\Delta \mathbf{u} = \operatorname{div} \operatorname{grad} \mathbf{u}$$

Constitutive parameters

$$\mathbf{e} = [\gamma_{11}, \gamma_{22}, \gamma_{33}, \gamma_{12}, \gamma_{21}, \gamma_{23}, \gamma_{32}, \gamma_{31}, \gamma_{13}, \kappa_{11}, \kappa_{22}, \kappa_{33}, \kappa_{12}, \kappa_{21}, \kappa_{23}, \kappa_{32}, \kappa_{31}, \kappa_{13}]^T,$$

$$\mathbf{C} = \text{diag} \begin{bmatrix} \mathbf{C}_1 & \mathbf{C}_2 & \mathbf{C}_2 & \mathbf{C}_2 & \mathbf{C}_3 & \mathbf{C}_4 & \mathbf{C}_4 & \mathbf{C}_4 \end{bmatrix},$$

$$\mathbf{C}_1 = \begin{bmatrix} \lambda + 2\mu & \lambda & \lambda \\ \lambda & \lambda + 2\mu & \lambda \\ \lambda & \lambda & \lambda + 2\mu \end{bmatrix}, \quad \mathbf{C}_3 = \begin{bmatrix} \alpha + 2\beta & \alpha & \alpha \\ \alpha & \alpha + 2\beta & \alpha \\ \alpha & \alpha & \alpha + 2\beta \end{bmatrix},$$

$$\mathbf{C}_2 = \begin{bmatrix} \mu + \mu_c & \mu - \mu_c \\ \mu - \mu_c & \mu + \mu_c \end{bmatrix}, \quad \mathbf{C}_4 = \begin{bmatrix} \beta + \gamma & \beta - \gamma \\ \beta - \gamma & \beta + \gamma \end{bmatrix}.$$

$$\mu > 0, \quad 3\lambda + 2\mu > 0, \quad \mu_c > 0, \quad \beta > 0, \quad 3\alpha + 2\beta > 0, \quad \gamma > 0.$$

Stiffness ratio Ω_b in pure bending of a beam with circular cross-section with radius a

$$\Omega_b = 1 + \frac{8N^2}{1 + \nu} \left[\frac{1 - (\beta - \gamma)/(\beta + \gamma)}{(\delta a)^2} + \frac{[(\beta - \gamma)/(\beta + \gamma) + \nu]^2}{\zeta(\delta a) + 8N^2(1 - \nu)} \right],$$

$$\delta^2 = 4\mu_c\mu/(\beta + \gamma)(\mu + \mu_c)$$

$$\zeta(x) = \frac{x^2(xI_0(x) - I_1(x))}{xI_0(x) - 2I_1(x)},$$

I_0, I_1 the modified Bessel functions of the first kind

Krishna-Reddy and Venkatasubramanian 1978

