

Zero Emission Building Envelopes - Comparison of Different Wall Constructions in a Life Cycle Perspective

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Background

- This work is part of the research program *Robust Envelope Construction Details for Buildings of the 21st Century* (ROBUST)
- There is a large potential for energy efficiency in buildings. In this context, insulation of the building envelope is a major contributor, both regarding energy efficiency and cost.
- When only energy use during operation of the building is considered, it will always be beneficial to increase the amount of insulation. However, when greenhouse gas (GHG) emissions during the life cycle is the evaluation criteria, the increased use of materials will at some stage equalize the benefits of reduced energy use during operation.

Objective

- This work presents a case study, where the effect of changing the insulation thickness of a wall is evaluated regarding GHG-emissions during the life cycle.
- The wall is a typical wood frame wall with glass wool, which is located in a house which fulfils the Norwegian energy regulations from 2010.
- The house is assumed to be located in Trondheim, Norway.
- The effect of changing the emission factor for the energy source has also been evaluated.
- The main question is: **Is there an optimum insulation thickness, and how do the emission factors influence the results?**

Description of house

Dimensions (internal)

Length x Width: 10 m x 8 m

Height: 5 m (2 floors)

Heated floor area: $A_{BRA} = 160 \text{ m}^2$

Heated air volume: $V = 384 \text{ m}^3$

External walls

Internal area including windows and door: $A_{wall} = 180 \text{ m}^2$

Internal area excluding windows and door: $A_{wall\ net} = 148 \text{ m}^2$

Thermal transmittance: $U_{wall} = 0.087 - 0.652 \text{ W}/(\text{m}^2\text{K})$, depending on insulation thickness

Windows and door

Total area of windows and door: $A_{wd} = 32 \text{ m}^2$ ($A_{wd}/A_{BRA} = 20 \%$)

Thermal transmittance of windows and door: $U_{wd} = 1.2 \text{ W}/(\text{m}^2\text{K})$

Roof

Internal area: $A_{roof} = 80 \text{ m}^2$

Thermal transmittance: $U_{roof} = 0.13 \text{ W}/(\text{m}^2\text{K})$

Floor

Internal area: $A_{floor} = 80 \text{ m}^2$

Thermal transmittance: $U_{floor} = 0.15 \text{ W}/(\text{m}^2\text{K})$

Thermal bridges

Normalized thermal bridge value: $\psi'' = 0,03 \text{ W}/(\text{m}^2_{BRA}\text{K})$

Description of house

Air tightness

Air changes at 50 Pa: $n_{50} = 2.5 \text{ h}^{-1}$

Ventilation system

CAV ventilation

Heat exchanger efficiency: $\gamma_{\text{he}} = 80 \%$

Ventilation rate: $V_V = 192 \text{ m}^3/\text{h}$

Specific Fan Power: $\text{SFP} = 2.5 \text{ kW}/(\text{m}^3\text{s})$

Heating and cooling

Electrical heating system

Maximum effect for heating (including heating of ventilation air): $P_h = 10400 \text{ W}$

Heating efficiency: $\gamma_h = 100 \%$

No cooling

Internal loads

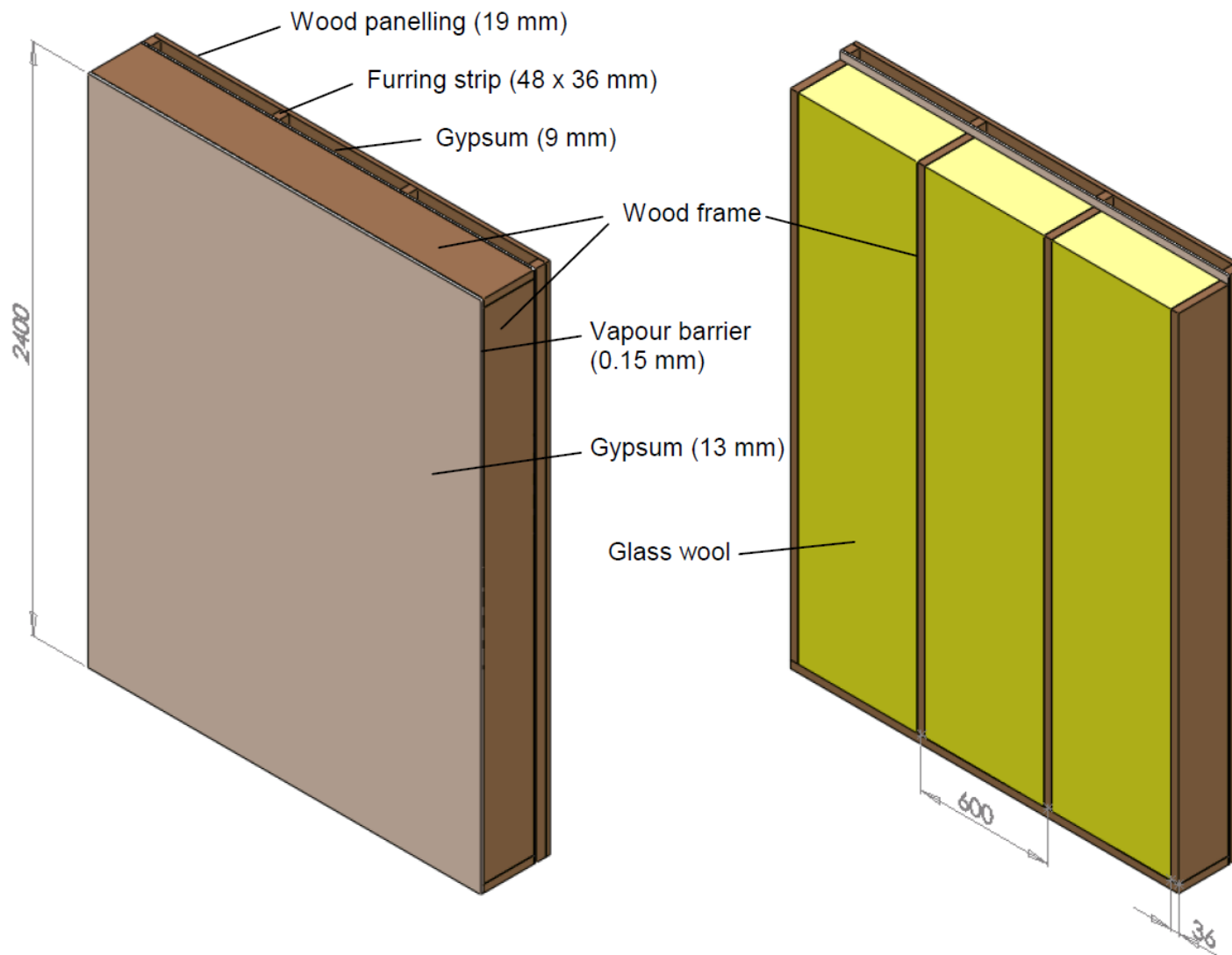
Lighting during operational hours (16/7/52): $P_l = 312 \text{ W}$ (312 W heat gain)

Technical equipment during operational hours (16/7/52): $P_t = 480 \text{ W}$ (288 W heat gain)

Domestic hot water: $P_{\text{dhw}} = 544 \text{ W}$ (0 W heat gain)

Heat gain due to people: 240 W

Description of wall



Methodology

The reduction of GHG-emissions, related to reduced heating demand, when the insulation thickness of the wall is increased with one unit:

$$\Delta GHG(t_m)_{Operation} = \frac{(E_{t1} - E_{t2})KT}{(t_2 - t_1)A_{wall\ net}} \quad (1)$$

The increase of GHG-emissions, related to increased use of materials, when the insulation thickness of the wall is increased with one unit:

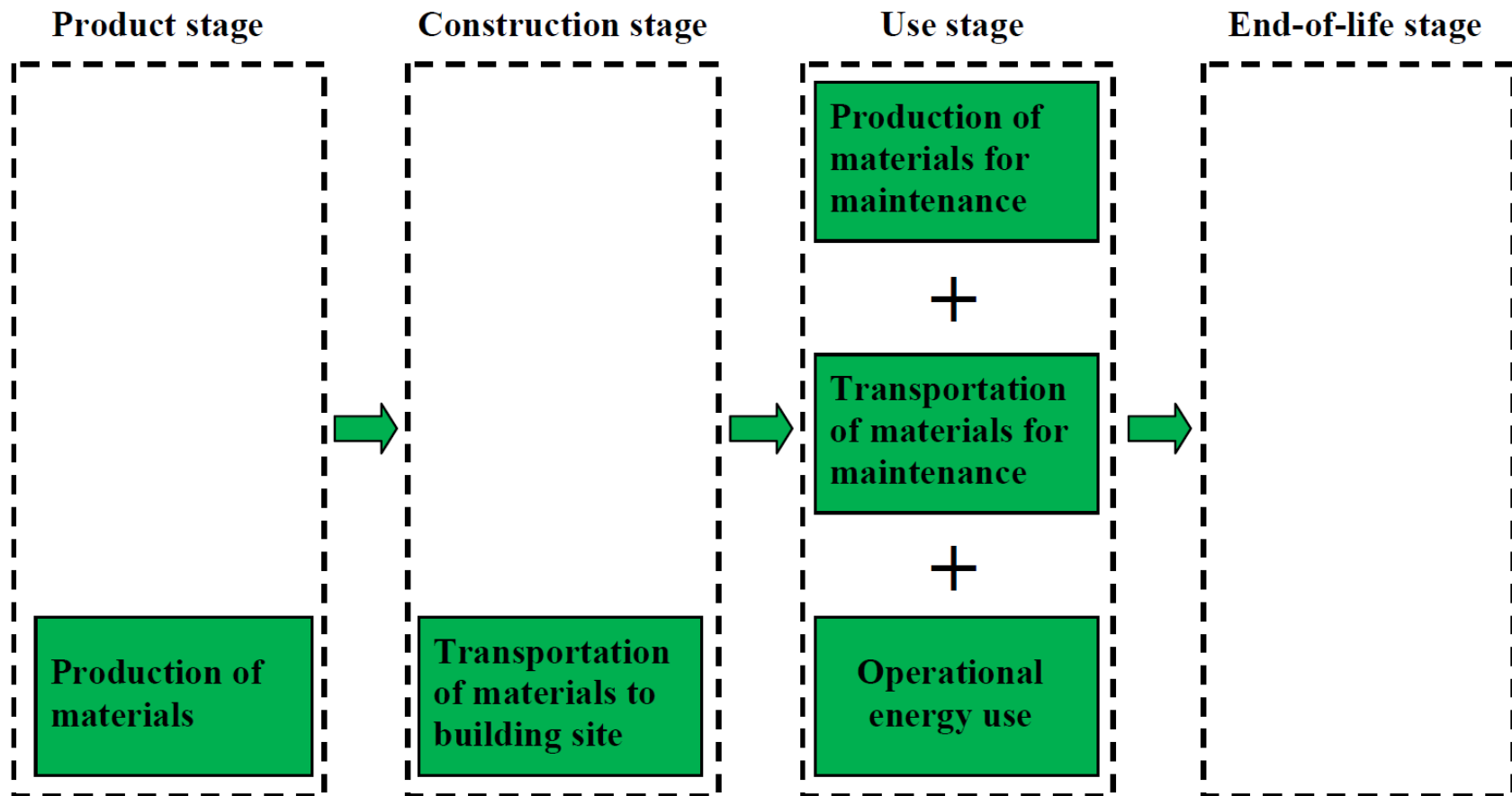
$$\Delta GHG(t_m)_{Materials} = \frac{GHG_{Materials\ t2} - GHG_{Materials\ t1}}{(t_2 - t_1)A_{wall\ net}} \quad (2)$$

The optimum point of reduced heating demand versus increased use of materials:

$$\Delta GHG(t_m)_{Operation} = \Delta GHG(t_m)_{Materials} \quad (3)$$

LCA – System boundaries

In this simplified life cycle assessment, only the following processes were included:



LCA – Production of materials

- Emission data for production of the materials was taken from Klimagassregnskap.no.
- The electricity specific part of the emissions related to production of the materials can be adjusted according to a user specified emission factor for electricity.
- Since there is no official emission factor for electricity from the Norwegian grid, and there are different arguments for which factor to use, the analyses have been carried out with 0.010, 0.050, 0.200, 0.400 and 1.000 kg CO₂ eq/kWh.

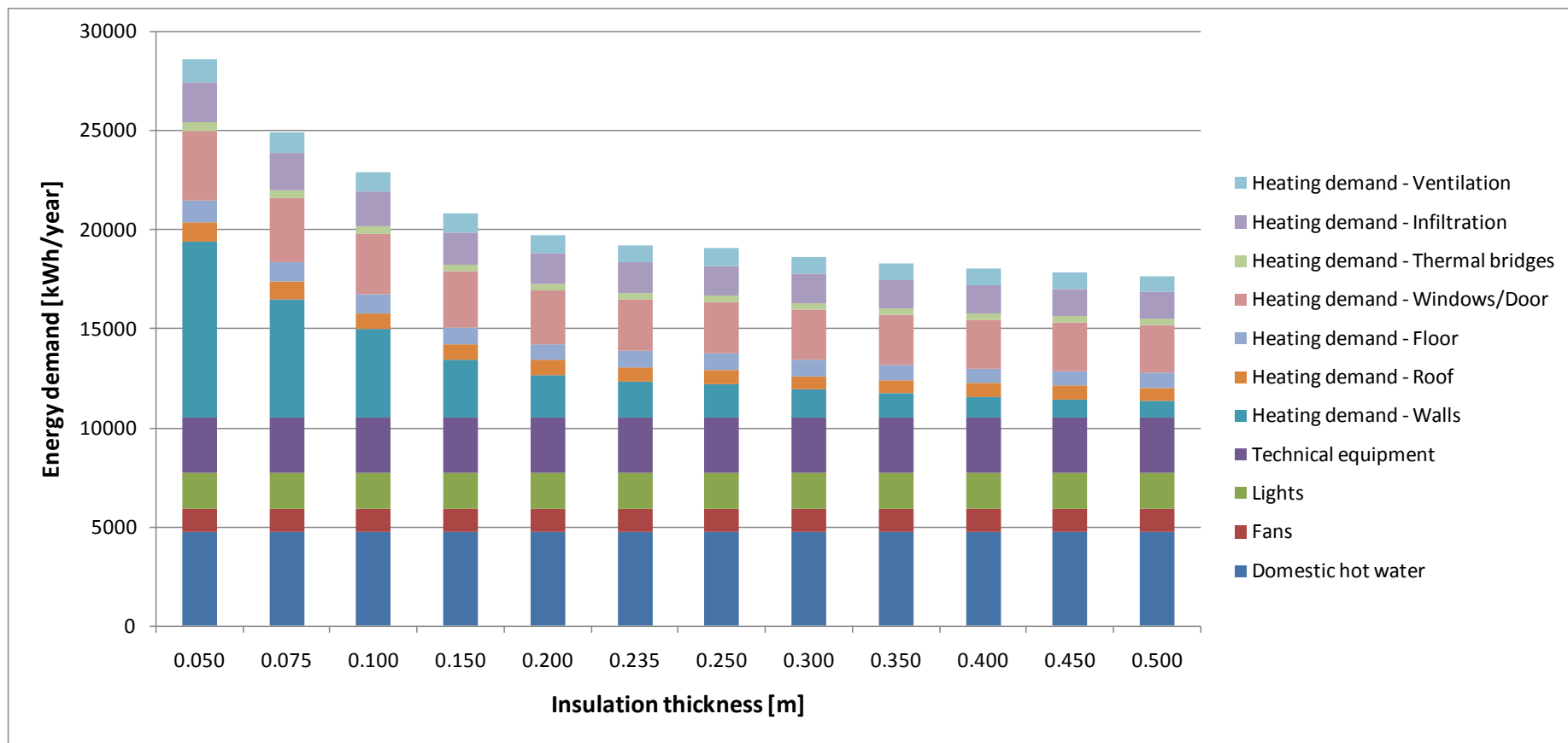
LCA – Transportation

The emission factor for transportation was taken from Klimagassregnskap.no.

The emissions per m² wall are calculated on basis of the following assumptions:

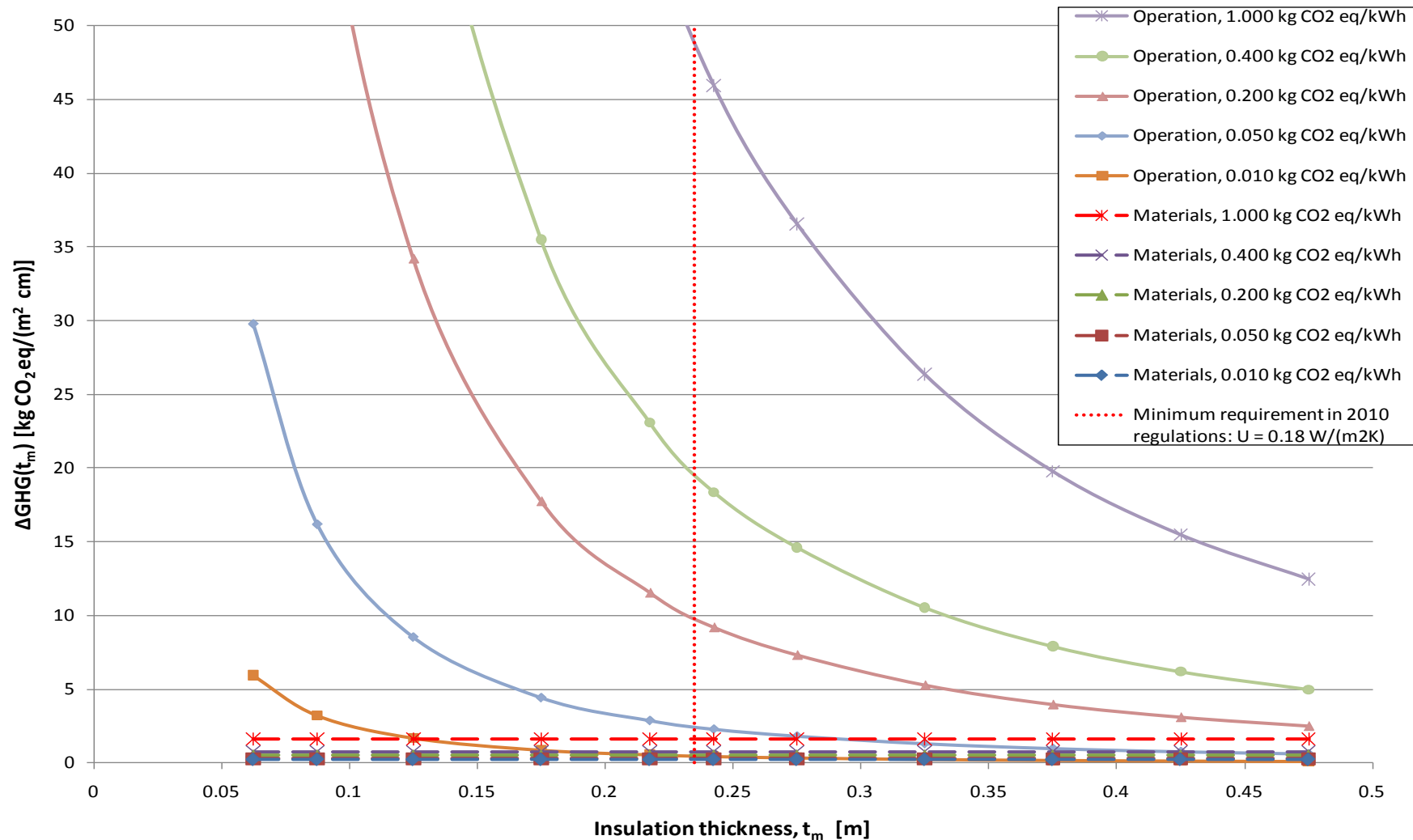
1. The travel distance from the manufacturer to the building site is 1000 km.
2. The maximum load capacity is 30000 kg for all the materials except the glass wool.
3. The maximum load capacity is 37 pallets with 3.7 m³ glass wool per pallet.

LCA - Energy demand and emission factors

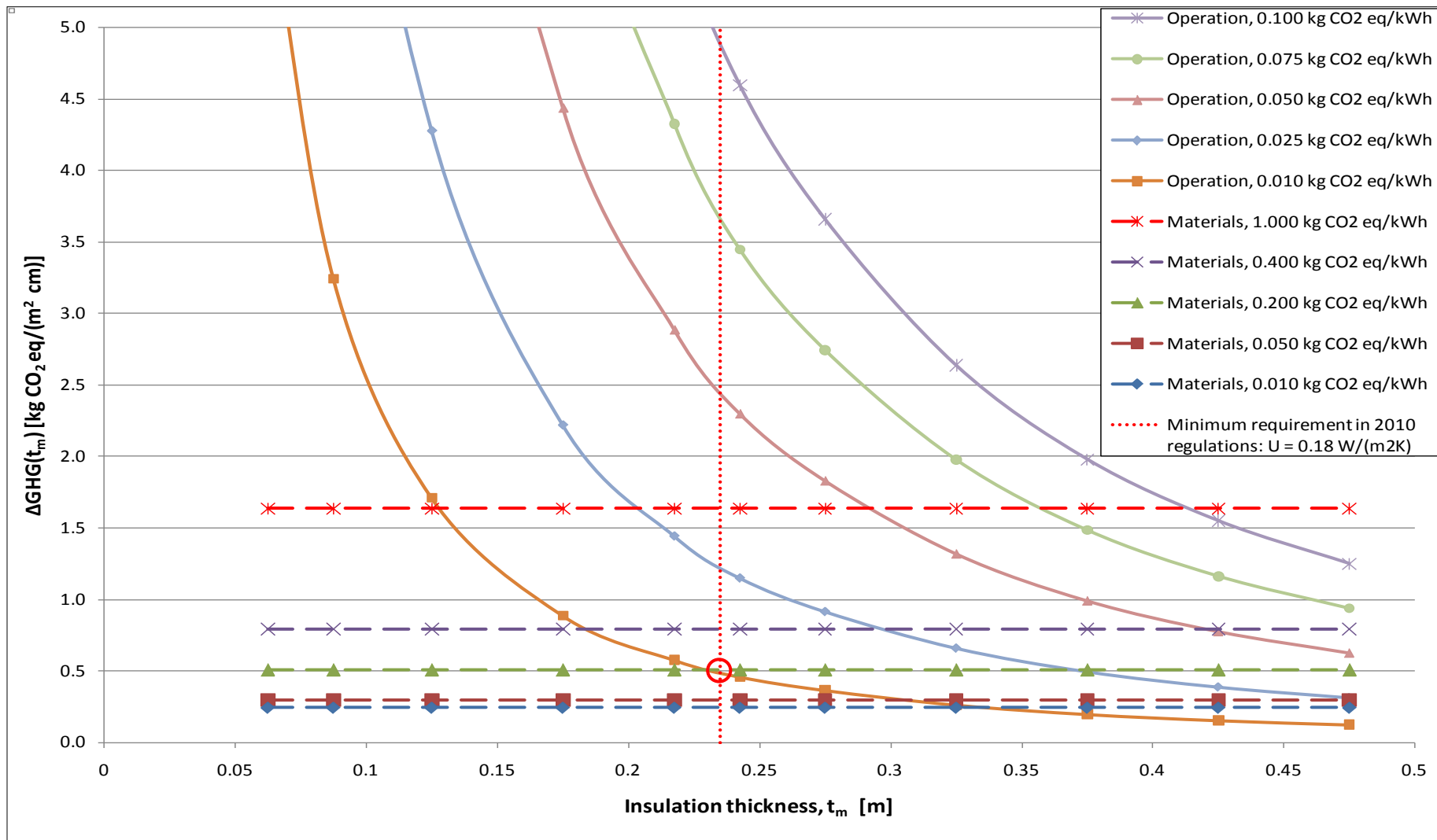


- Emission factors: 0.010, 0.025, 0.050, 0.075, 0.100, 0.200, 0.400 and 1.000 kg CO₂ eq/kWh.

Results



Results



Conclusions

- The energy sources and the corresponding emission factors are of great importance when the optimum insulation thickness is determined on basis of GHG-emissions (CO₂-equivalents) during the life cycle.
- Increased insulation thickness is always beneficial as long as the emission factor for the energy supply to the building is above 0.200 kg CO₂ eq/kWh.
- There is an optimum insulation thickness between 0.050 m and 0.500 m when the emission factor for the energy supply to the building is below 0.100 kg CO₂ eq/kWh. The specific optimum insulation thickness depends upon the combination of emission factors.

Recommendations for further work

- Different combinations of wall structures and energy supply systems should be investigated.
- The effect of cooling demand should be investigated.

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