



Numerical Simulation of Building Components : Towards an Efficient Implementation of Air Convection in HAM-models

Jelle Langmans, Ralf Klein, Staf Roels
Division of Building Physics
Departement of Civil Engineering
K.U.Leuven, Belgium

Andreas Nicolai, John Grunewald
Instituts für Bauklimatik,
Technical University of Dresden, Germany

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‘Low energy building’, built in 2009



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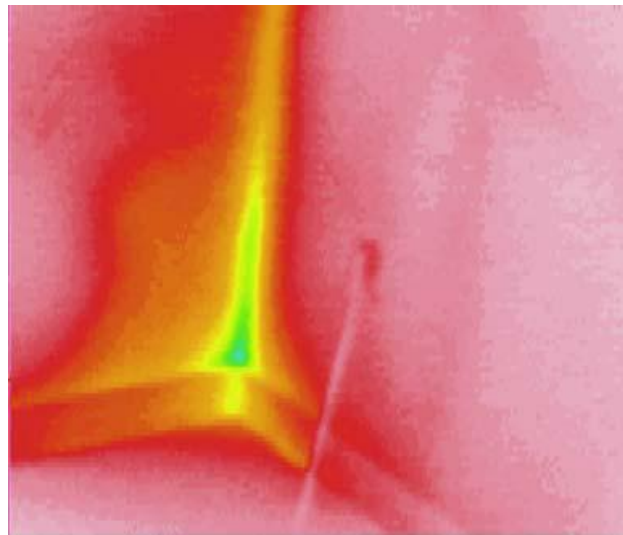
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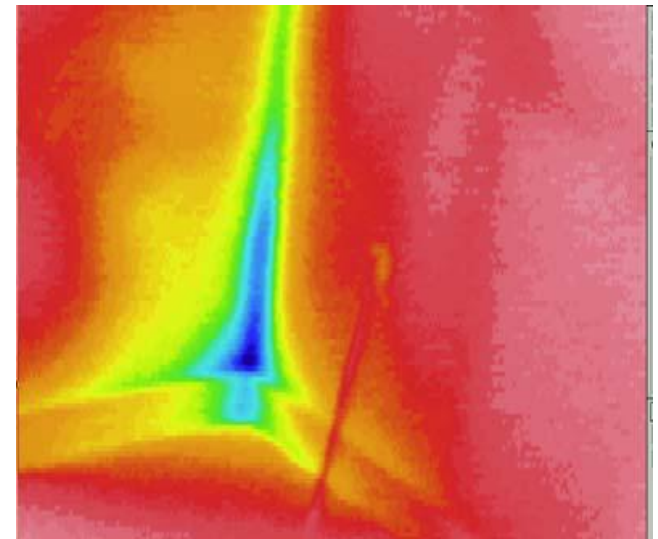
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No pressure



Under pressure



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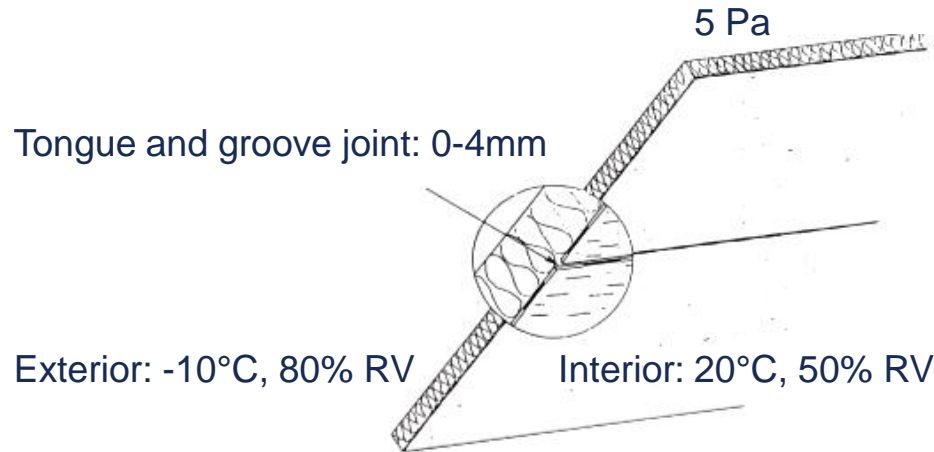
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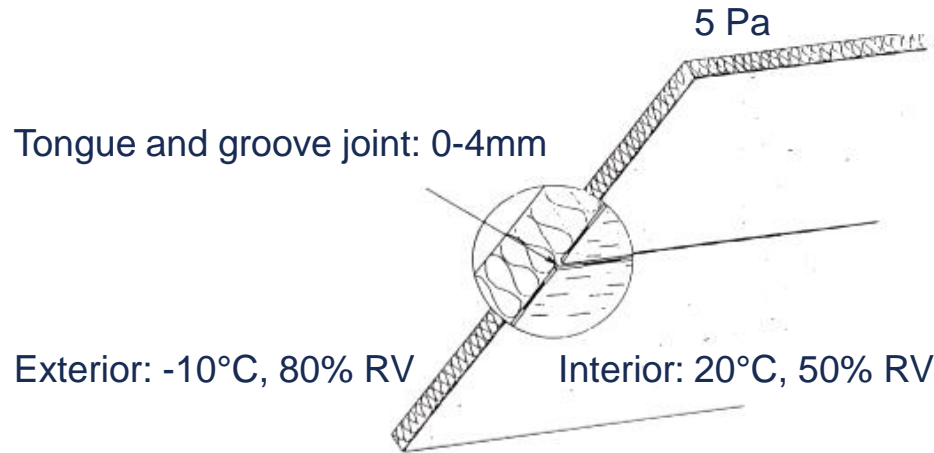
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CONVECTION VS DIFFUSION





	DIFFUSION		
Vapour diffusion resistance	$\mu_d=100m$	$\mu_d=50m$	$\mu_d=3$
Daily diffusion transport (g/m ²)	0,15	0,3	5
	CONVECTION		
Joint (mm)	0mm	2mm	4mm
Daily convection transport (g/m)	9	39	144



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HAM-models including air transport are scarce



Efficient implementation of air convection in HAM-models



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$$\mathbf{H} \quad \frac{\partial u}{\partial t} = - \frac{\partial}{\partial x_k} \left[q_{cond} + h_v j_{diff}^v + h_w j^w \right]_k + \Sigma \dot{u}$$

A

$$\mathbf{M} \quad \frac{\partial \rho^{w+v}}{\partial t} = - \frac{\partial}{\partial x_k} \left[j_{diff}^v + j^w \right]_k$$



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$$\mathbf{H} \quad \frac{\partial u}{\partial t} = - \frac{\partial}{\partial x_k} \left[q_{cond} + h_v (j_{diff}^v + j_{conv}^v) + h_w j^w + h_a j^a \right]_k + \Sigma \dot{u}$$

$$\mathbf{A} \quad \frac{\partial \rho^a}{\partial t} = - \frac{\partial}{\partial x_k} [j^a]_k$$

$$\mathbf{M} \quad \frac{\partial \rho^{w+v}}{\partial t} = - \frac{\partial}{\partial x_k} [j_{diff}^v + j_{conv}^v + j^w]_k$$



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$$\mathbf{H} \quad \frac{\partial u}{\partial t} = - \frac{\partial}{\partial x_k} \left[q_{cond} + \left(h_v (j_{diff}^v + j_{conv}^v) + h_w j^w \right) + h_a j^a \right]_k + \Sigma \dot{u}$$

$$\mathbf{A} \quad \frac{\partial \rho^a}{\partial t} = - \frac{\partial}{\partial x_k} \left[j^a \right]_k$$

$$\left(\mathbf{M} \quad \frac{\partial \rho^{w+v}}{\partial t} = - \frac{\partial}{\partial x_k} \left[j_{diff}^v + j_{conv}^v + j^w \right]_k \right)$$



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$$\mathbf{H} \quad \frac{\partial u}{\partial t} = - \frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u}$$

$$\mathbf{A} \quad \frac{\partial \rho^a}{\partial t} = - \frac{\partial}{\partial x_k} [j^a]_k$$


$$j^a = -\rho_a \frac{k_a}{\eta} \left(\frac{\partial p_a}{\partial x_k} + \rho_a g \cos \alpha \right)$$



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Previous attempts/approaches



Fully coupled approach (Delphin 4)

$$\frac{\partial \rho^a}{\partial t} = - \frac{\partial}{\partial x_k} [j^a]_k$$

$$(c_m \rho_b + c_a \rho_a) \frac{\partial T}{\partial t} = - \frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u}$$

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Fully coupled

$$\frac{\partial P_a}{\partial t} = \frac{k_a}{c_a} \nabla^2 P_a$$
$$\frac{\partial T}{\partial t} = \frac{\lambda}{\rho c} \nabla^2 T$$

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Fully coupled

6.8 m²/s

$$\frac{\partial P_a}{\partial t} = \frac{k_a}{c_a} \nabla^2 P_a$$

1.1 10⁻⁶ m²/s

$$\frac{\partial T}{\partial t} = \frac{\lambda}{\rho c} \nabla^2 T$$

Example for rock wool*

$$c_a = 1,2 \cdot 10^{-5} \text{ kg/m}^3 \cdot \text{Pa}$$

$$k_a = 8 \cdot 10^{-5} \text{ s}$$

$$\rho c = 33600 \text{ J/K} \cdot \text{m}^3$$

$$\lambda = 0.036 \text{ W/mK}$$

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Previous attempts

Fully coupled

6.8 m²/s

$$\frac{\partial P_a}{\partial t} = \frac{k_a}{c_a} \nabla^2 P_a$$

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> 6 000 000

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Quasi steady state approach (Delphin 5)

$$\cancel{\frac{\partial \rho^a}{\partial t}} = - \frac{\partial}{\partial x_k} [j^a]_k$$

$$(c_m \rho_b + c_a \rho_a) \frac{\partial T}{\partial t} = - \frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u}$$

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Quasi steady state approach

$$0 = -\frac{\partial}{\partial x_k} [j^a]_k$$

$$(c_m \rho_b + c_a \rho_a) \frac{\partial T}{\partial t} = -\frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u}$$

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Quasi steady state approach

$$\text{DAE} \left\{ \begin{array}{l} 0 = -\frac{\partial}{\partial x_k} [j^a]_k \\ (c_m \rho_b + c_a \rho_a) \frac{\partial T}{\partial t} = -\frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u} \end{array} \right.$$

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Quasi steady state approach

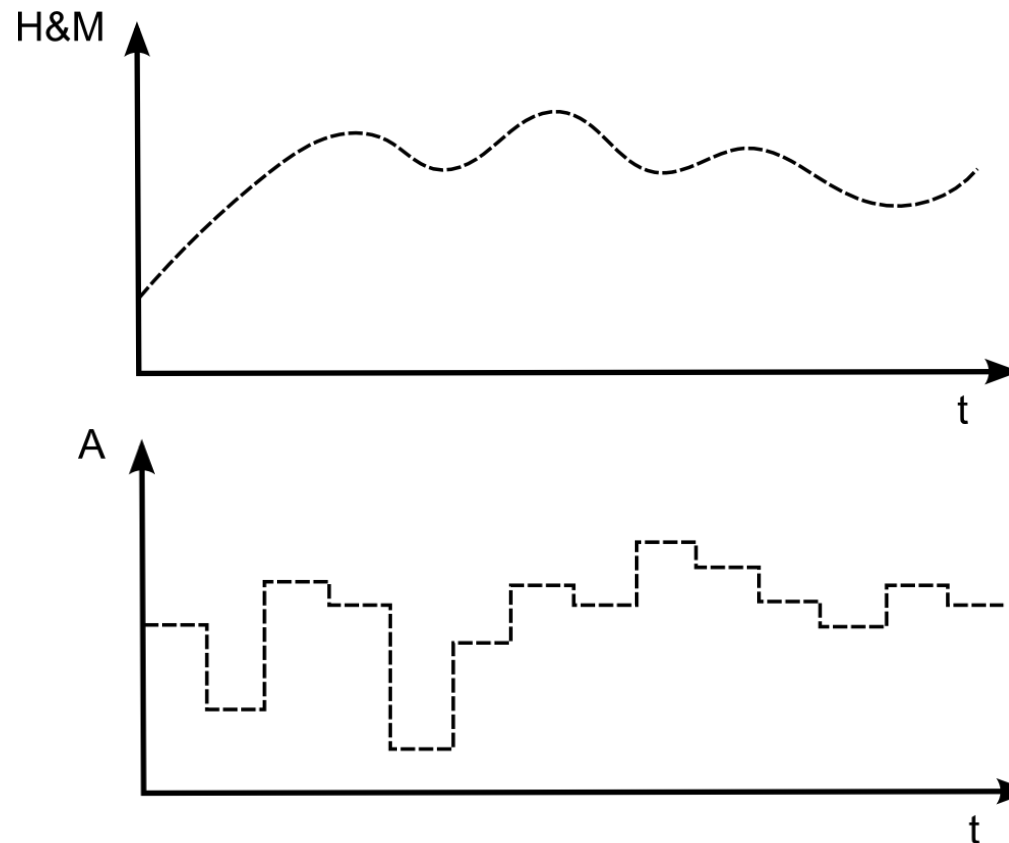
$$\text{DAE} \left\{ \begin{array}{l} 0 = -\frac{\partial}{\partial x_k} [j^a]_k \\ (c_m \rho_b + c_a \rho_a) \frac{\partial T}{\partial t} = -\frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u} \end{array} \right.$$

General form of the ODE integrator: $\dot{y} = f(t, y)$



Previous attempts

Quasi steady state



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Quasi steady state

- Good simulation performance
- Perfect solution for forced convection problems
- Might lead to numerical instability for buoyant dominated problems

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Governing equations

$$0 = -\frac{\partial}{\partial x_k} [j^a]_k$$

$$(c_m \rho_b + c_a \rho_a) \frac{\partial T}{\partial t} = -\frac{\partial}{\partial x_k} [q_{cond} + h_a j^a]_k + \Sigma \dot{u}$$

Transport equations

$$j^a = -\rho_a \frac{k_a}{\eta} \left(\frac{\partial p_a}{\partial x_k} + \rho_a g \cos \alpha \right)$$

$$q_{cond} = -\lambda \frac{\partial T}{\partial x}$$



Numerical solution method

Finite Volume Method (FVM)

↳ System PDE transformed to DAE

Discretization:

Diffusion terms: central-difference

$$(q_{cond})_{L,i} = -\lambda_{L,i} \frac{T_i - T_{i-1}}{0.5(\Delta x_{i-1} + \Delta x_i)}$$

Convective terms: upwind scheme

$$(h_a j^a)_{L,i} = \begin{cases} (h_a)_{i-1} j^a & j^a > 0 \\ (h_a)_i j^a & j^a \leq 0 \end{cases}$$



Numerical solution method

$$F(t, y, \dot{y}) = 0$$

$$y = [p_{a,0}, u_0, p_{a,1}, u_1, \dots, p_{a,n}, u_n]^T$$

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Numerical solution method

$$F(t, y, \dot{y}) = 0$$

$$y = [p_{a,0}, u_0, p_{a,1}, u_1, \dots, p_{a,n}, u_n]^T$$



DAE-solver: IDA



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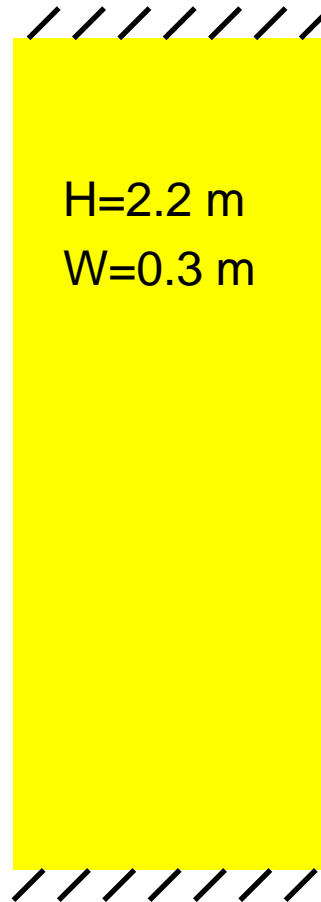
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Natural convection in a porous media: vertical / horizontal layer

Kohonen, 1985



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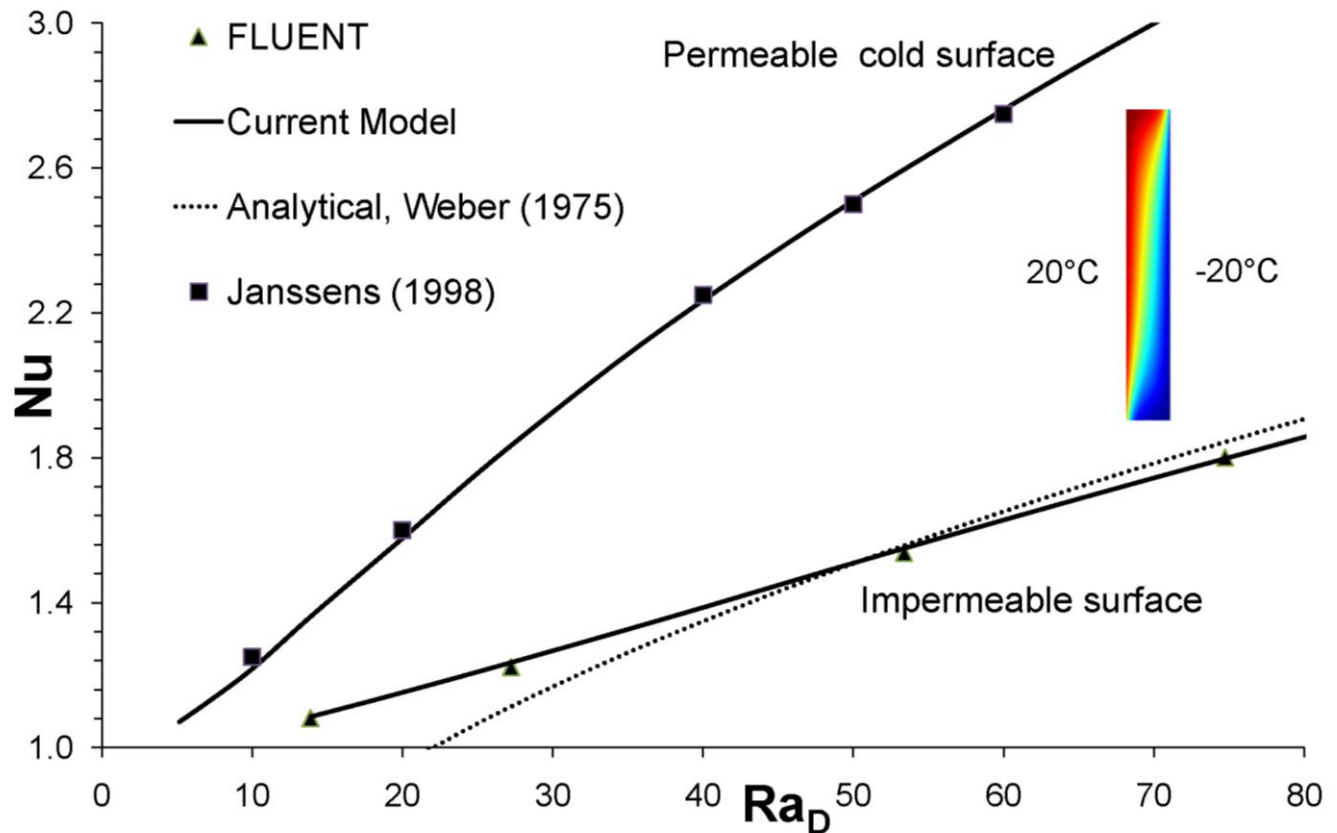
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$$Nu = \frac{Q_{tot}}{Q_{cond}} = \frac{Q_{tot}}{H\Delta T\lambda_x / D}$$

$$Ra_D = g\beta D\Delta T \left(\frac{\rho c}{\nu} \right) \frac{k_x}{\lambda_x} \frac{4a_k}{\left(\sqrt{a_\lambda} + \sqrt{a_k} \right)^2}$$



Vertical Layer



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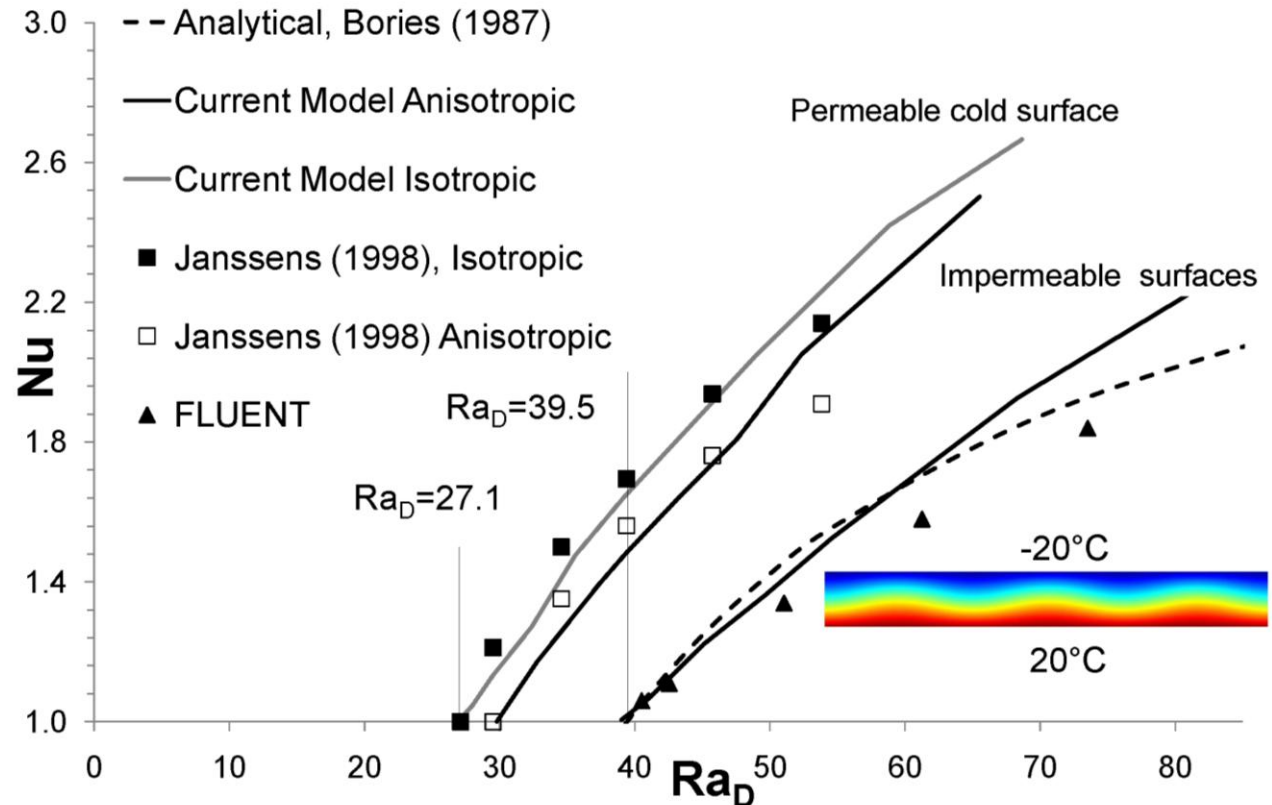
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Horizontal Layer



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- Implementation of air transport in Delphin HAM tool
- Previous approaches were discussed
- A new approaches using DAE solver
- Validation

