

Rising Damp in Historic Buildings: The Wall Base Ventilation System

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1. Introduction

Rising damp

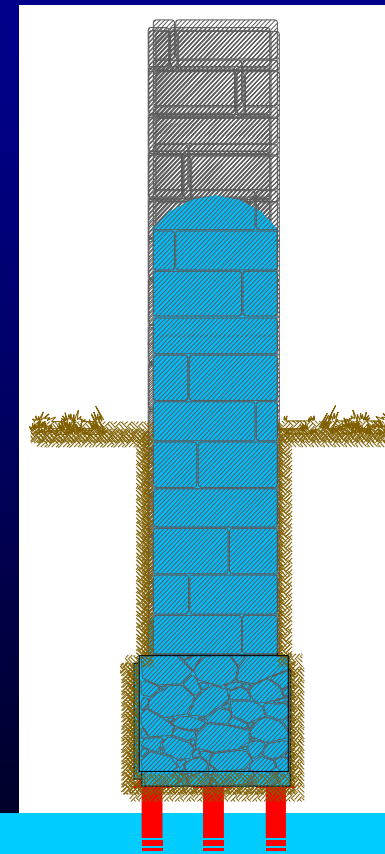


One of the main causes of old buildings degradation

Limitations of traditionally used technologies in thick walls with heterogeneous composition



New solutions



1. Introduction



Rising Damp: Major cause of decay to masonry material: stone, brick, mortar

The conservation of historical buildings assumes a considerable importance



1. Introduction

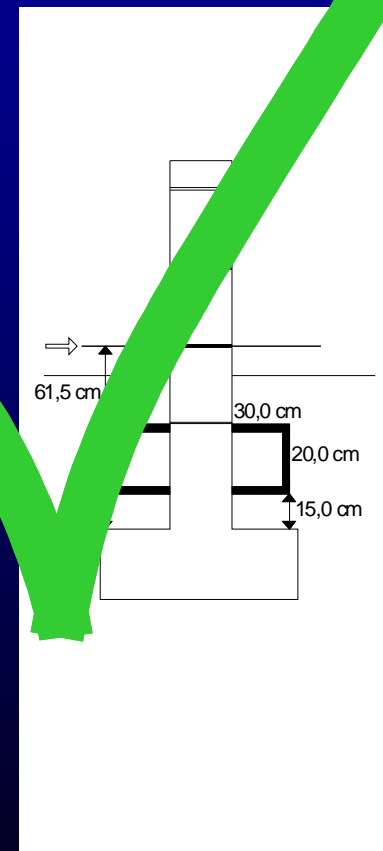
Building Physics Laboratory (LFC)

Faculty of Engineering of
University of Porto (FEUP)



Wall Base Ventilation System

HUMIVENT



1. Introduction

HUMIVENT

Understand the behaviour of air within the conduct

Calculate the water flow removed from the wall

Estimate the front level archived with the system

Aims:

- Develop a model:
describe and characterize the water vapour transport over the conduct, between the wall and the conduct
the relation with the front level on the wall
- Validate the model



2. Analytical Analyse - Wall

2.1 Theory

Hall and Hoff (2002)

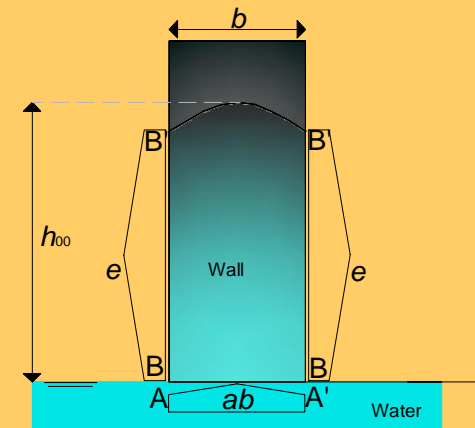
Absorption inflow and evaporation loss in balanced
(Disregarding gravitational forces)

$$b \frac{di}{dt} = b \frac{S}{2} t^{-1/2} - eh$$

$$i = \theta_w h$$

$$h = S \sqrt{\frac{b}{2e\theta_w} \left[1 - \exp\left(-\frac{2e}{b\theta_w} t\right) \right]}$$

$$h_{\infty} = S \sqrt{\frac{b}{2e\theta_w}}$$



- b** wall thickness (m)
- i** volume of liquid absorbed (m³/m²)
- θ_w** liquid bulk volume (-)
- t** time (s)
- S** sorptivity coefficient (m/s^{1/2})
- e** evaporation potential (m/s)
- h** rising damp height (m)



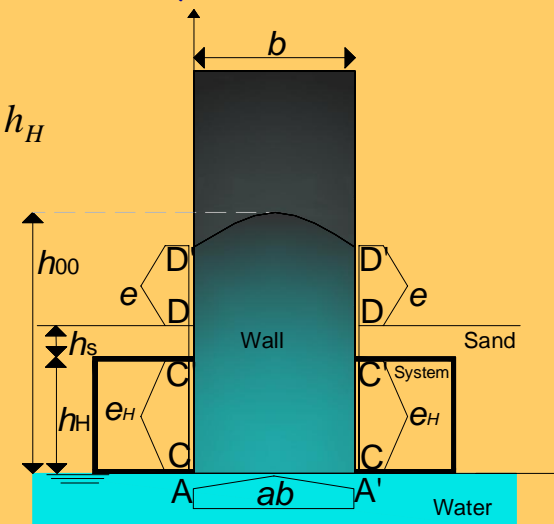
2. Analytical Analyse - Wall

2.2 Our contribution

Absorption inflow and evaporation loss in balanced
(Disregarding gravitational forces)

$$\frac{bS^2}{2\theta_w h_\infty} = e(h_\infty - h_s - h_H) + e_H h_H$$

- b wall thickness (m)
- θ_w liquid bulk volume (-)
- S sorptivity coefficient (m/s^{1/2})
- e evaporation potential (m/s)
- e_H evaporation potential (HUMIVENT system) (m/s)
- h_s height of the sand (m)
- h_H height of the HUMIVENT system (m)



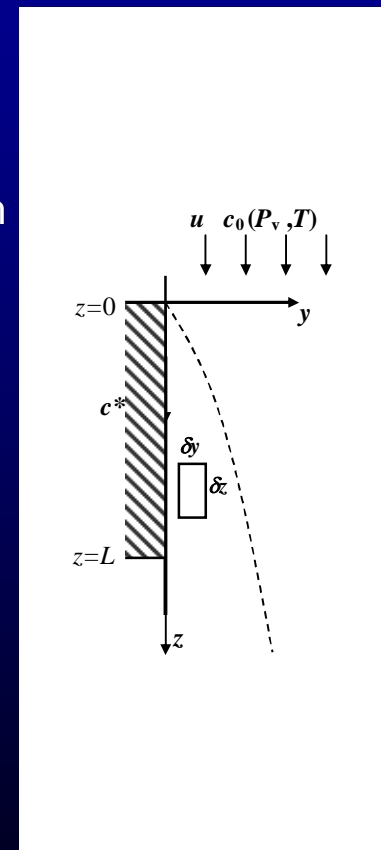
$$h_\infty = \frac{h_s}{2} + \left(1 - \frac{e_H}{e}\right) \frac{h_H}{2} + \sqrt{\frac{bS^2}{2\theta_w e} + \frac{h_s^2}{4} + \left(\frac{e_H}{e} - 1\right)^2 \frac{h_H^2}{4} + \left(1 - \frac{e_H}{e}\right) \frac{h_s h_H}{2}}$$



3. Analytical and Numerical Analyse - System

It is consider:

- A system along which air is flowing, close to the saturated wall ($0 < z < L$)
- Air flow will be taken to be steady, with uniform average velocity u
- Concentration of water vapour in the air fed to the channel is c_0
- Concentration of water vapour in the solid wall is c^*
- Situations for which the moisture transfer boundary layers is thin



Steady state material balance leads to:

$$u \frac{\partial c}{\partial z} = D_m \frac{\partial^2 c}{\partial y^2} + D_m \frac{\partial^2 c}{\partial z^2}$$



3. Analytical and Numerical Analyse - System

If is consider:

Wall surface, is a surface of constant concentration

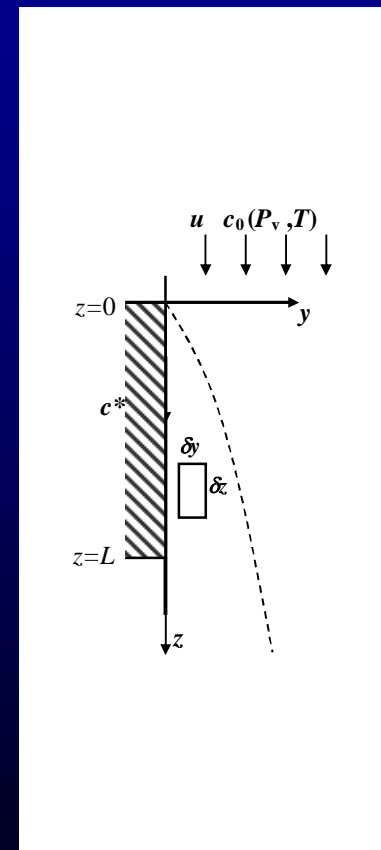
Equation of diffusion in one dimension

Analytical solution

$$e_H = \frac{(c^* - c_0)}{\rho_w} \left(\frac{4D_m}{\pi L/u} \right)^{1/2}$$

Steady state material balance leads to:

$$u \frac{\partial c}{\partial z} = D_m \frac{\partial^2 c}{\partial y^2} + D_m \frac{\partial^2 c}{\partial z^2}$$



3. Analytical and Numerical Analyse - System

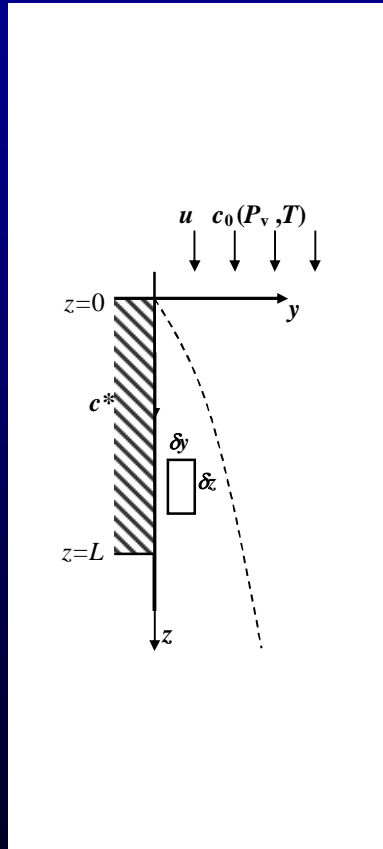
Finite-difference method

Numerical solution

$$e_H = \frac{(c^* - c_0)}{\rho_w} \left(\left(\frac{2D_m}{\pi L / u} \right)^{1/4} + \frac{4D_m}{\pi L / u} \right)^{1/2}$$

Steady state material balance leads to:

$$u \frac{\partial c}{\partial z} = D_m \frac{\partial^2 c}{\partial y^2} + D_m \frac{\partial^2 c}{\partial z^2}$$



4. Experimental Study

Assess the effect of the HUMIVENT system

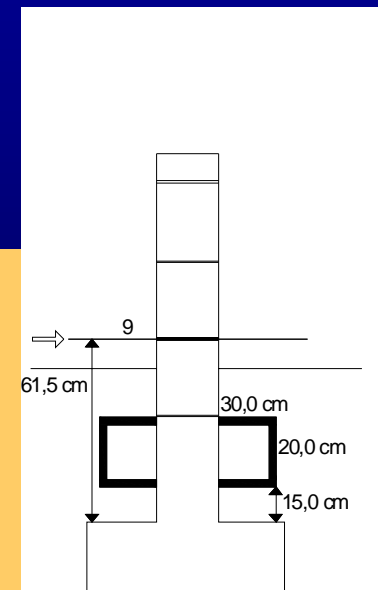


Flow entrance:

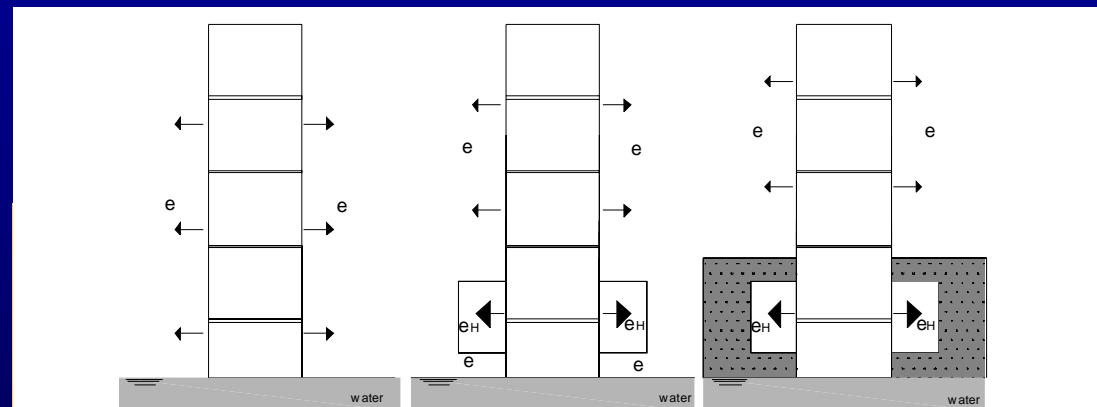
- Temperature
- Relative Humidity

Flow exit:

- Temperature
- Relative Humidity



4. Experimental Study

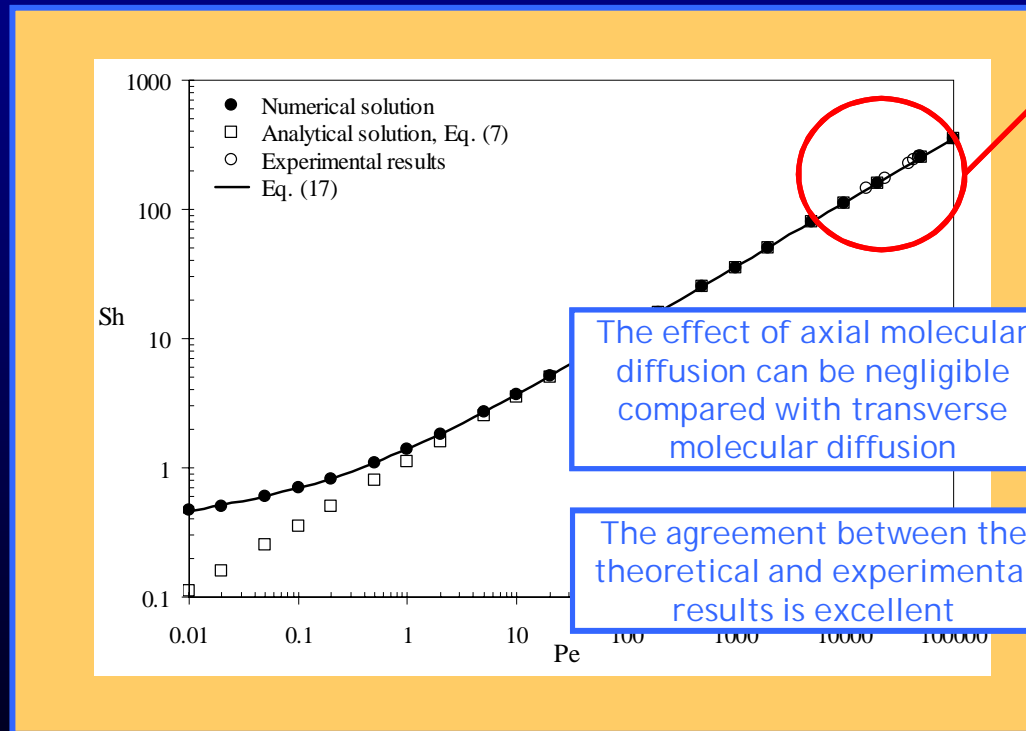


Configuration 1	Configuration 2		Configuration 3	
RH_0 (%)	RH_0 (%)	RH_s (%)	RH_0 (%)	RH_s (%)
60.0	57.8	60.1	58.2	60.3
T_0 (°C)	T_0 (°C)	T_s (°C)	T_0 (°C)	T_s (°C)
20.0	22.6	22.4	23.0	22.8



5. Results and Discussion

1st - Analytical and Numerical Analyse - System



Experimental results

Numerical



Analytical



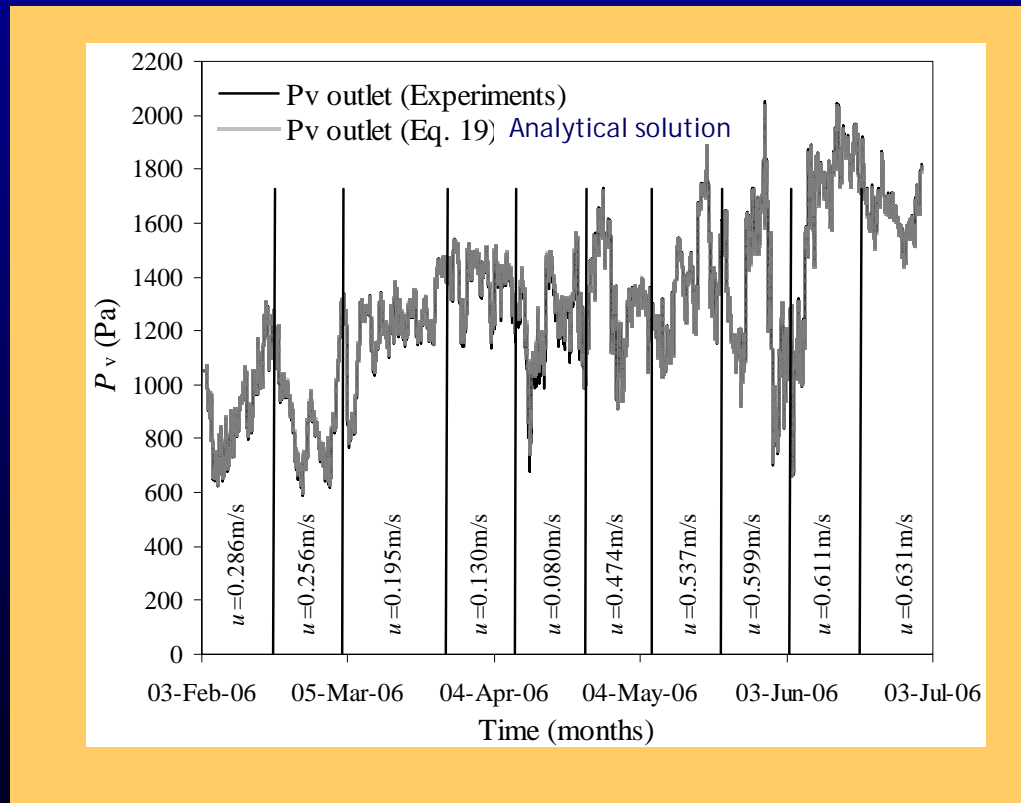
Experimental

do not deviate by more than 1%



5. Results and Discussion

2nd - Analytical and Numerical Analyse - System and Experimental Results



The agreement between the theoretical and experimental results is excellent:

Over the entire range

For all tested velocities

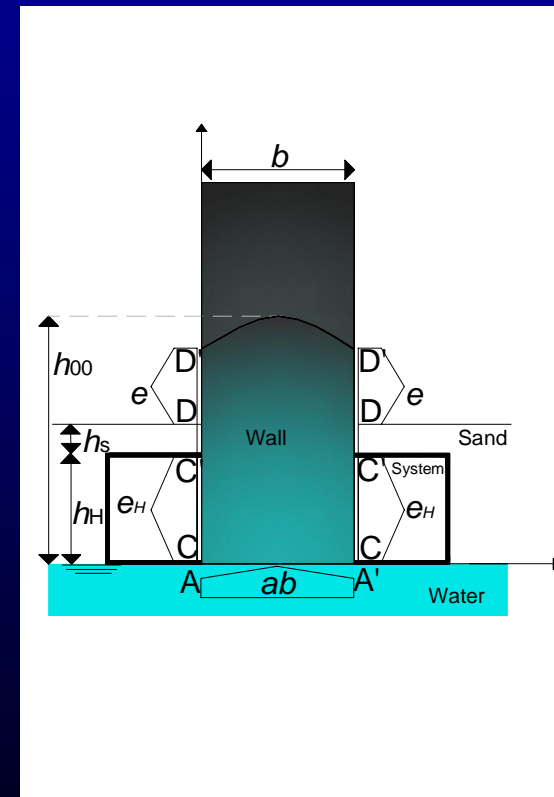
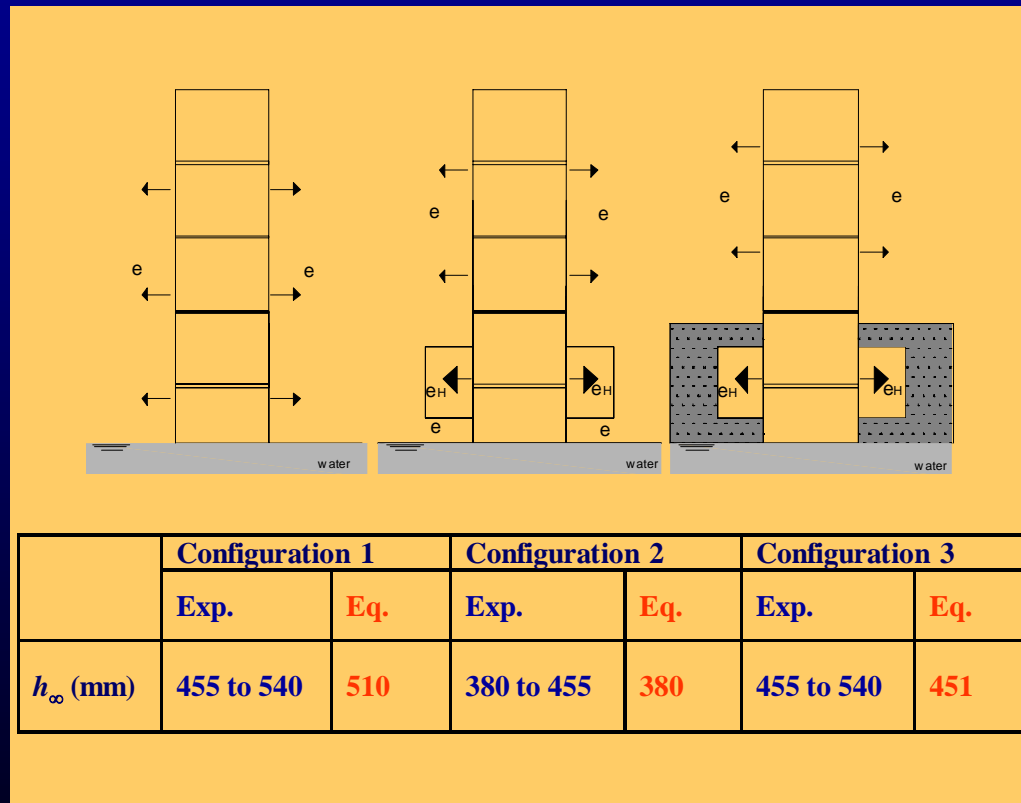
For all tested inlet condition

During this research
HUMIVENT
removed water from the wall



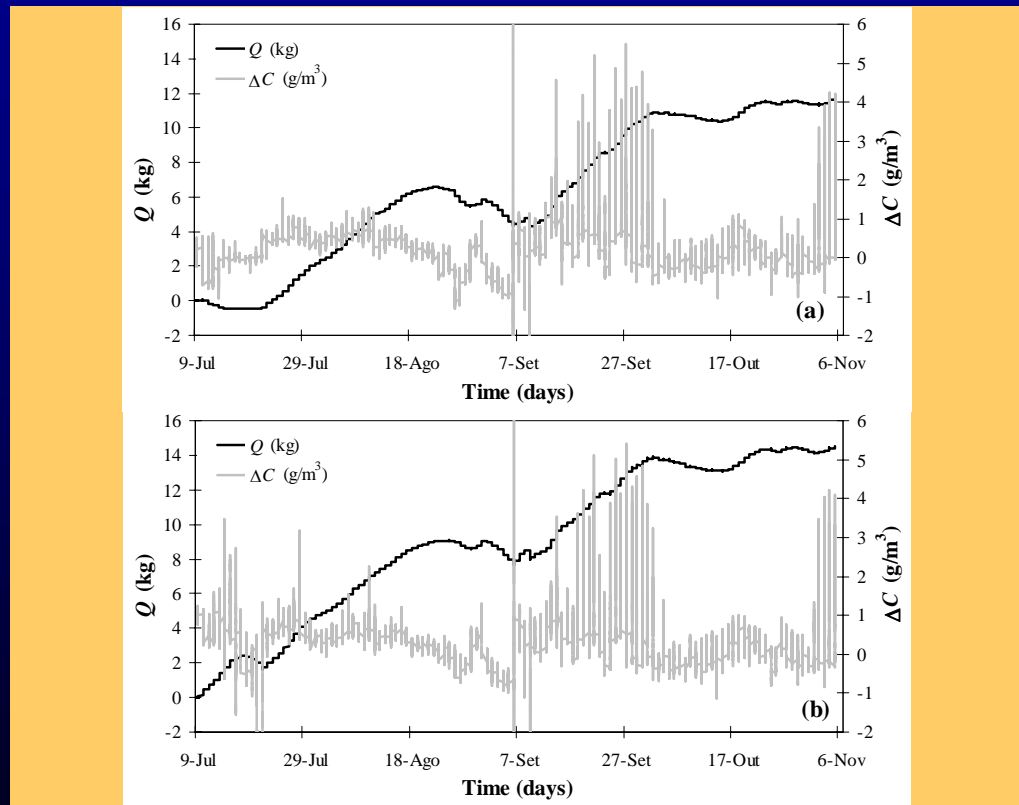
5. Results and Discussion

3rd - Analytical Analyse - Wall and System



5. Results and Discussion

3rd - Analytical Analyse - Wall and System



Quantity of water vapour extracted and concentration differential in:
(a) - Configuration 2,
(b) - Configuration 3.

During these months of experimental research, in laboratory tests on Configurations 2 and 3 the new treatment technique extracted approximately 11.8 kg and 14.5 kg of water respectively



In field ...



A.S. Guimarães, J.M.P.Q. Delgado and V.P. de Freitas
NSB - 9th Nordic Symposium on Building Physics
1st June, Tampere, Finland , 2011

Buildings where, for the first time,
HUMIVENT was applied - PORTUGAL



6. Conclusions

Wall base ventilation is a simple technique that has a great practical potential

Before treatment



After treatment

HUMIVENT



6. Conclusions

- Moisture transfer between a wall surface and the air flowing along it, lends to a theoretical analysis
- The equations resulting from differential moisture balance has been numerically and analytically solved
- The numerical and analytical similar results let conclude that the axial molecular diffusion effect can be negligible compared with transverse molecular diffusion



6. Conclusions

- The excellent agreement between the theoretical and experimental results allocate the use of the develop equations to estimate the evaporative process
- The model of rising damp that predicts steady height of rise are consistent with laboratory observations, which provide a good validation of the analysis
- Using this model it is possible to scale the HUMIVENT system, optimise it and predict its behaviour.

HUMIVENT
Prototype



Thank you for your attention

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